Predicting Local Transport Coefficients at Solid-Gas Interfaces

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Abstract

The regular nanoporous structure make zeolite membranes attractive candidates for separating molecules on the basis of differences in transport rates (diffusion). Since improvements in synthesis have led to membranes as thin as several hundred nanometers by now, the slow transport in the boundary layer separating bulk gas and core of the nanoporous membrane is becoming increasingly important. Therefore, we investigate the predictability of the coefficient quantifying this local process – the surface permeability α – by means of a two-scale simulation approach. Methane tracer-release from the one-dimensional nanopores of an AFI-type zeolite is employed. Besides a pitfall in determining α on the basis of tracer exchange, we, importantly, present an accurate prediction of the surface permeability using readily available information from molecular simulations. Moreover, we show that the prediction is strongly influenced by the degree of detail with which the boundary region is modeled. It turns out that not accounting for the fact that molecules aiming to escape the host structure must indeed overcome two boundary regions yields too large a permeability by a factor of 1.7 to 3.3, depending on the temperature. Finally, our results have far-reaching implications for the design of future membrane applications.

Keywords: surface barrier, transmission coefficient, molecular simulation, Monte Carlo, TST.

Introduction

Molecular exchange between a gas reservoir and a nanoporous crystalline solid (e.g., a zeolite membrane or crystal) represents a key design process in applications, such as adsorption, molecular-sieving, catalysis, and ion-exchange. Over the last few decades, a good understanding has been developed with regard to the role 1 and dependence 2,3,3-7 of guest diffusion in such regular host structures, that is, the transport mechanism of molecules inside the nanopores far away from the interface to the fluid phase. 8,9 For example, gas diffusion in zeolites is known to be an activated process 4-7 where molecules need to overcome a series of regularly distributed internal diffusion barriers which arise from nanopore shape in the unit-cell alone. Many phenomena, including the loading-dependence of the self-diffusion coefficient, can be explained by the variation of such (free) energy barriers. In this context, molecular simulations have been proven to be invaluable, 4,5,10 owing to improved agreement with experiments. 11-13 Despite these accomplishments, there are still unresolved problems, 14 many of which are related to the boundary layer separating the gas-phase region from the core zeolite space.

While cases exist in which the boundary layer may accelerate molecular exchange between the reservoir and the porous host, ^{15,16} it usually slows down the transport rate close to the surface, ^{6,7,17–20} leading to the name of this phenomenon: surface barriers. Exciting insights into their nature have been unraveled only recently. ^{6,7,20} Microscopy experiments ⁶ in conjunction with mesoscopic modeling ⁷ evidenced that exceptionally few accessible pore entrances together with a large number of lattice defects (i.e., vast crystal non-idealities as depicted in Figure 1a) formed extremely high surface barriers on very large MOF Zn(tbip) crystals (labeled "defect barriers" here). On the other hand, we have recently shown with the aid of molecular simulations ²⁰ that perfect single-crystal zeolite membranes (i.e., highly ideal crystal and surface structure) can also possess strong barriers at the external surface, as long as thin membranes (\lesssim 100 unit cells) are being considered. The origin of these barriers lay in the difference of the mean field experienced by the guest molecules in gas and adsorbed phase (Figure 1b), for which reason they are labeled intrinsic barriers in the following. Therefore, a unique source of surface barriers does obviously not exist,

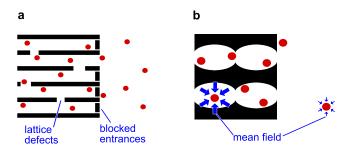


Figure 1: Surface barriers can have different reasons. Blocked pore entrances together with lattice defects (a) and mean-field differences (b) "felt" by molecules in adsorbed and gas space, respectively, can both render the rate of transport at the solid-gas interface extremely small.

- emphasizing the necessity of a consequent discrimination between different effects.
- Despite the improvement of understanding different sources of surface barriers, an assessment of the coefficient quantifying the rate of transport in the boundary layer the surface permeability α is so far possible to a satisfactory degree for the defect barriers only. In numerous case studies, Kärger, Chmelik, and co-workers 6,17,18,21,22 successfully measured the surface permeabilites of gas molecules in large crystals. However, the consistent prediction of this coefficient for intrinsic surface barriers via information from molecular simulations is a challenging task to date. $^{19,23-25}$ This paper therefore aims at highlighting a pitfall that might have been overlooked so far and, most importantly, to provide a satisfying prediction of the surface permeability over those conditions that are currently of practical interest.

38 Methodology

- 39 We focus on the conceptually simplest case of molecular exchange tracer exchange where
- macroscopic concentration gradients are absent and the exchange involves differently "colored"
- 41 molecules rather than different species (Figure 2a and movie in Supporting Information). Since
- tracer exchange situations correspond directly to self-diffusion, all diffusion coefficients presented
- here are self-diffusivities (D_S) .
- Several steps are necessary for molecules to be exchanged between zeolite space and gas-phase
- region, as illustrated by the trajectory of a single molecule in Figure 2a:

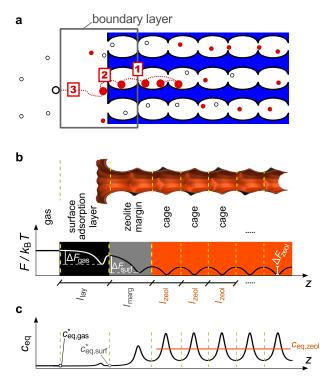


Figure 2: a) Exchange of a tracer molecule involves three steps: 1. Diffusion to reach the outermost cage (zeolite margin). 2. Jumping out of the pore structure to reach the external surface adsorption layer. 3. Finally, leaving this layer to disappear in the gas phase. b) Channel and surface structure of the here studied AFI-type zeolite together with a representative free-energy profile, $F/k_{\rm B}T$, along the exchange direction, z. c) Equilibrium concentration profile, $c_{\rm eq}$, corresponding to b); note that $c_{\rm eq}(z) = \exp[-F(z)/k_{\rm B}T] \times {\rm const.}$

- 1. A molecule needs to traverse the nanopore to eventually reach the outermost cage referred to as the zeolite margin in the remainder. This intracrystalline diffusion is impeded by successive barriers originating from the repetitive crystal structure (internal diffusion barriers, ΔF_{zeol} , as seen at the end of the orange region of Figure 2b).
- 2. The molecule must then get out of the pore and reside on the external surface adsorption layer. This process is controlled by a first boundary barrier, ΔF_{surf} (grey region in Figure 2b).
- 3. Finally, to truly desorb from the solid and thus to loose the color, the molecule must overcome a second boundary barrier, $\Delta F_{\rm gas}$, that separates the surface adsorption layer from the gas-phase region, as evidenced by Figure 2b (black region).
- Step 1 is mathematically described by the standard Fickian diffusion equations. Step 2 and 3 are

usually modeled with a surface evaporation boundary condition, 26 yielding a relationship between the current net flux of tracer molecules at the boundary, $j_{\text{surf}}(t)$, the surface permeability and the driving force:

$$j_{\text{surf}}(t) = \alpha \cdot [c_{\text{surf}}(t) - c_{\text{surf}}(t \to \infty)], \tag{1}$$

where c denotes concentration of tracer (i.e., colored) molecules and $c_{surf}(t \to \infty) = 0$ in the present case because we consider complete exchange. At this point, a first problem arises because we obviously need to describe two different processes (steps 2 and 3) with a single coefficient (α), which represents one of the main tasks of the present work. However, we consider the release in the first part of the analysis to proceed via a one-step mechanism in which molecules are assumed to be exchanged when they have performed step 2 in Figure 2a. This is instructive because the approximation has been made often in the past but it is not free of problems, as mentioned earlier. Moreover, the resulting one-step surface permeability prediction helps in fact rationalizing the final 2-step permeability.

The example of methane desorbing from siliceous AFI-type zeolite membranes will be em-68 ployed, the structure ²⁷ of which exhibits one-dimensional channels (Figure 2b). The methodology introduced in Ref. 20 is extended, as described in detail in the Supporting Information (SI1). It briefly comprises of two stages each involving a different maximum length scale: (i) moleculardetailed simulations where AFI membranes of ≈5 nm thickness are used, and (ii) a continuum calculation to reach membranes of up to several micrometer width. The first stage, where methane is modeled as a united atom, ²⁸ yields free-energy and concentration profiles (Figure 2) from which the input data to the second stage are extracted, notably equilibrium transport rates between the different compartments (zeolite cages, margin, surface adsorption layer) as well as their equilibrium concentrations and widths. In the second stage, the material balances are solved numerically on 77 the basis of the data obtained from the molecular simulations. These calculations provide us with transient concentration profiles (Figure 3a). Integral tracer-release curves, 1 - m(t)/m(0), are then determined (Figure 3b), describing the progress of exchanging "colored" molecules (red circles in Figure 2a) for "uncolored" molecules (open circles). Such exchange curves are commonly encountered in diffusion-experiment analysis, ²⁹ and they can be envisioned in an integral modeling approach to pressure swing adsorption. ³⁰

The release curves are fitted to the analytical solution²⁶ of Fick's laws under consideration of the evaporation boundary condition (Eq. 1):

$$1 - \frac{m(t)}{m(0)} = 1 - \sum_{i=1}^{\infty} \frac{2L^2 \exp[-\gamma_i^2 D_{S} t / (\delta/2)^2]}{\gamma_i^2 (\gamma_i^2 + L^2 + L)},$$
(2)

with $L=(\delta/2)\alpha/D_{\rm S}$, δ the membrane thickness, and γ_i are the positive roots of $\gamma \tan \gamma = L$.

The thus obtained transport coefficients are plotted in Figure 3c and d for increasing membrane thickness and a single state point (T,p). Note again that these results are obtained from one-step release calculations.

The here presented two-stage simulation strategy features two distinct advantages. First, simulations with membrane thicknesses up to the micrometer range become feasible which would not be possible with conventional equilibrium molecular dynamics (MD), 23 let alone non-equilibrium MD 31 employing thick zeolite membranes. Second, the condition of tracer exchange avoids the possibility that the surface permeability is process-dependent, that is, whether molecule release or uptake is being investigated (cf., Supporting Information SI2 and Ref. 18). Therefore, we can focus on the concentration dependence of the permeability which is indeed speculated to be the reason why α varies for uptake and release in non-equilibrium conditions. 18

Results

99 One-Step Release Mechanism

It might seem trivial to match the surface permeability from the continuum calculation with predictions based solely on information from the first stage (molecular simulations). Figure 3 shows however that both D_S and α are dependent on the membrane thickness for a given state point. Theoretically, the parameters must not vary with membrane thickness. When we repeat the continuum

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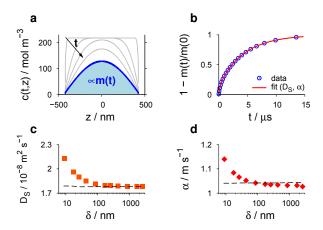


Figure 3: Concentration profiles (a) obtained from a continuum calculation (one-step release mechanism, δ =848 nm) yield the tracer-exchange curve (b). The fitted self-diffusion coefficients (c) and surface permeabilities (d) depend in fact on the membrane thickness, δ . (T=181 K, p=1202 Pa).

simulations by setting the zeolite margin width equal to the cage separation $(l_{\text{marg}} = l_{\text{zeol}})$ and 104 also equating the equilibrium concentration in the margin with the one of the bulk-zeolite space 105 $(c_{\text{eq.marg}} = c_{\text{eq.zeol}})$, the horizontal dashed lines in Figure 3 are obtained, where the diffusivity 106 equals the prediction by dynamically corrected transition state theory. 19,32-34 With these assump-107 tions, the transport coefficients do not change with thickness, illustrating an important point. The 108 dependence of the transport coefficients on the membrane thickness is brought about by subtle 109 differences of the properties of the zeolite margin from the properties of the inner cages. The max-110 imal deviation of D_S and α amounts to 20% and 10%, respectively. This underlines the necessity for an improved analytical integral solution of the diffusion process incorporating varying margin width and equilibrium concentration into the boundary condition. The effect, however, can so far not have had any immediate implication to membranes that are currently producible because their thicknesses³⁵ are yet more than a magnitude apart from the region where it becomes significant. 115 But it will come into play in the future because improvements in membrane synthesis adumbrate 116 constantly decreasing thicknesses. 36,37 117

The practically relevant membrane width range is several hundred nanometers and onwards ^{35,37} for which both transport coefficients show asymptotic values (Figure 3c and d). This means that the determination of the surface permeability would involve an entire set of continuum calculations to

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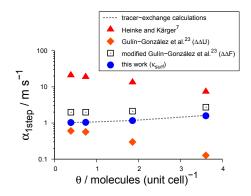


Figure 4: Surface permeability as a function of loading (T=181 K), obtained from the two-stage simulation approach (line) used in the present work to mimic tracer-exchange experiments. Permeability predictions using information from the first – the molecular – simulation stage only are presented as symbols where different models are tested. Note, first, that the main difference between the modified estimate by Gulín-González et al. 23 and our prediction lies in κ_{surf} because of the earlier mentioned relationship of free energy and concentration and, second, the molecules are assumed being exchanged when they arrived on the external surface adsorption layer (one-step desorption mechanism).

identify when α becomes constant or, alternatively, a long simulation with a very thick membrane. Instead, one wants to skip this stage and calculate α directly based on data of the first (molecular-122 level) stage. In this context, we tested three different models. Figure 4 summarizes the results 123 where the symbols represent the model predictions and the line the (target) surface permeability 124

from the tracer-exchange continuum calculations with very thick membranes.

The first model (triangles in Figure 4) was suggested by Kärger and co-workers ^{6,7} and assumes 126 that the surface permeability is proportional to the diffusion coefficient ($\alpha = 0.5 \cdot D_{\rm S}/l_{\rm zeol}$). While 127 the surface permeability obtained from the tracer-exchange calculations increases with loading 128 (line), the model predicts a declining trend of α because the corresponding diffusion coefficient 129 decreases with loading. Hence, the model of Kärger et al. is not applicable for the here studied sys-130 tems. Since it was validated against diffusion experiments probing defect barriers, the qualitative discrepancy emphasizes again the imperative of discriminating between different surface-barrier sources. As a consequence, different local transport coefficients are obtained just naturally, depending on the relative significance of the two different influences (intrinsic vs. defect barriers).

Gulín-González et al.²³ suggested that a correlation between the two transport coefficients

should be corrected by inclusion of an additional *potential*-energy barrier. This is, because a molecule experiences a higher barrier, $\Delta U_{\rm surf}$, when hopping out from the marginal cage onto the
external surface in comparison to the internal diffusion barriers, $\Delta U_{\rm zeol}$, [$\alpha = \exp(-\Delta \Delta U/k_{\rm B}T) \cdot D_{\rm S}/l_{\rm zeol}$, with $\Delta \Delta U = \Delta U_{\rm surf} - \Delta U_{\rm zeol}$]. However, this model does not lead to satisfactory qualitative results either (filled diamonds in Figure 4). What changes the trend of the permeability
prediction over loading is the consideration of higher free-energy barriers [$\alpha = \exp(-\Delta \Delta F/k_{\rm B}T) \cdot D_{\rm S}/l_{\rm zeol}$], labeled modified Gulín-González *et al.* in Figure 4 (squares). Still, a discrepancy is observed that is due mainly to the transmission coefficient, ^{19,20,38,39} $\kappa_{\rm surf}$, the significance of which
is discussed shortly. The accurate prediction of α (blue circles in Figure 4) follows

$$\alpha_{1\text{step}} = \bar{v} \times \kappa_{\text{surf}} \times c_{\text{eq,surf}}^* / c_{\text{eq,zeol}},$$
 (3)

where $\bar{v} = \sqrt{k_{\rm B}T/2\pi m_{\rm CH_4}}$ is the average velocity of the methane molecule in a single direction on the basis of kinetic gas theory, $c_{\rm eq,surf}^*$ is the equilibrium concentration of molecules at the location of the surface barrier and $c_{\rm eq,zeol}$ the average guest concentration inside the bulk-zeolite structure (\approx loading). The additional subscript "eq" facilitates discriminability between concentrations obtained from equilibrium c-profiles (i.e., time-invariant, as seen in Figure 2c) and transient concentrations which do change with time (Figure 3a).

Our surface-permeability prediction is in fact the equivalent to the self-diffusion coefficient estimate in the framework of dynamically-corrected transition state theory (dcTST). To realize this, consider the dcTST self-diffusivity: 32–34

$$D_{\rm S}^{\rm dcTST} = \bar{v} \times \kappa_{\rm zeol} \times \frac{\exp[-F(z_{\rm zeol}^*)/k_{\rm B}T]}{\int\limits_{\rm cage} \exp[-F(z)/k_{\rm B}T] dz} \times l_{\rm zeol}^2. \tag{4}$$

The equivalency of the terms $\bar{v} \times \kappa_i$ in eqs. 3 and 4 is obvious. Recalling that $c_{\rm eq} \propto \exp(-F/k_{\rm B}T)$ leads directly to the correspondence of the integral in the denominator divided by $l_{\rm zeol}$ and $c_{\rm eq,zeol}$, except for a factor which, however, is the same one between the two nominators and thus cancels

out exactly.

The role of the transmission coefficient is an important finding because, for predicting the 158 permeability, it is usually neglected that not 100% of the molecules having arrived on top of the 159 barrier between zeolite margin and surface adsorption layer will in fact end up on the external sur-160 face. The error introduced by assuming $\kappa_{\text{surf}} = 1$ amounts to a factor of 1.7...2.8 (cf., Supporting 161 Information SI3) which clearly manifests a profound quantitative impact on the final permeability 162 estimate. We furthermore point out that κ_{surf} may not simply be set to κ_{zeol} and that incorporating 163 κ_{surf} into the modified model by Gulín-González et al. still suffers from small deviations from the 164 tracer-exchange data because $\kappa_{\rm zeol}$ is dragged along in $D_{\rm S}$. Finally note also that α is a system 165 property that depends on the combination of guest molecule and host structure as well as on the properties of the surface and its immediate vicinity. ¹⁸

168 Two-Step Release Mechanism

The investigation of the one-step surface permeability has shed light on the peculiarities encountered when one aims at predicting α . Now we return to the case where the second exchange step is considered too, that is, a molecule must also leave the surface adsorption layer for the gas phase to be considered truly exchanged. Again, we determine the "target" $\alpha_{2\text{step}}$ from tracer-exchange calculations with thick membranes, with the difference that the surface adsorption layer is added in our continuum calculations. As seen from the excellent agreement between the thus obtained data (lines in Figure 5) and direct molecular-simulation predictions (large colored symbols), we find the two-step surface permeability to be given by:

$$\alpha_{2\text{step}} = \frac{\bar{v}/c_{\text{eq,zeol}}}{1/(\kappa_{\text{gas}}c_{\text{eq,gas}}^*) + 1/(\kappa_{\text{surf}}c_{\text{eq,surf}}^*)}$$
(5)

where $c_{\rm eq,gas}^*$ is the equilibrium concentration of molecules on the barrier between external surface adsorption layer and gas-phase region and $\kappa_{\rm gas}$ represents its corresponding transmission coefficient; note that $c_{\rm eq,gas}^* = c_{\rm eq,gas}$ (Figure 2c). The total surface permeability hence follows the be-

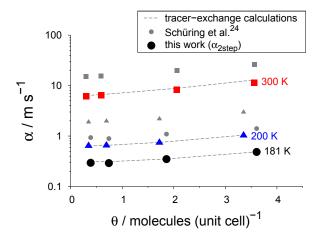


Figure 5: Surface permeability vs. loading for the case that tracer release included the desorption from the external surface adsorption layer (2-step release process). Results for various temperatures are shown, where the lines reflect data from the two-stage simulation approach mimicking tracer-exchange experiments and the symbols are predictions on the basis of readily available information from the first – the molecular – simulation stage only. The small grey symbols are surface permeability predictions due to Schüring $et\ al.^{24}$

havior of parallel resistances in electricity theory, that is, $\alpha_{2\text{step}} = 1/[1/(\alpha_{\text{gas}}) + 1/(\alpha_{1\text{step}})]$, when one defines $\alpha_{\text{gas}} \equiv \bar{v} \times \kappa_{\text{gas}} \times c_{\text{eq,gas}}^*/c_{\text{eq,zeol}}$.

The only alternative 2-step permeability prediction model that we have found is due to Schüring 182 et al.²⁴ (small grey symbols in Figure 5): $\alpha = P_{\text{enter}} \bar{v} / K$. K denotes the ratio of the average 183 concentrations in the zeolite margin and the bulk gas 24,25 and P_{enter} represents the fraction of 184 molecules that enter the zeolite of all molecules hitting on the surface in total. 40 While the model 185 captures the qualitative trend of increasing α with loading, it does not predict the permeability 186 quantitatively in a satisfactory manner. Deviations from the tracer-exchange calculations range 187 between 2.3 and 3.2, remaining significant even in case when the transmission coefficients (κ_{surf} 188 and κ_{gas}) are incorporated into the model (1.6...2.7). At this point, it is important to reiterate 189 that the tracer-exchange surface permeabilities for release and uptake are equivalent (Supporting 190 Information SI2).

Discussion

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A comparison between surface permeabilities obtained from the simplistic one-step and the more realistic two-step mechanism reveals that the external surface adsorption layer substantially retards the desorption from the membrane ($\alpha_{2\text{step}} \ll \alpha_{1\text{step}}$). The effect becomes the stronger, the lower the temperature gets, and amounts to a factor of $(\alpha_{1\text{step}}/\alpha_{2\text{step}})$ 1.7, 2.8, and 3.3 for T=300 K, 200 K, and 181 K, respectively. The comparison clearly underlines that the detailed structure of the membrane boundary layer is exceptionally important to obtain accurate permeability estimates. Since the accuracy is validated against tracer-exchange simulations rather than experiments, this fact deserves some final remarks. 200

The influence of the here reported intrinsic surface barriers on the permeability vanishes for the giant crystals⁴¹ employed in microscopy experiments.⁶ This is, because the measurements 202 are subject to spatial resolution limitations of around 0.5 µm (interference microscopy) and lar-203 ger (infrared microscopy), and consequently prohibiting the detection of intrinsic surface barriers which level off at this scale. ^{19,20} Nevertheless, the question arises to which extent *possible* defects 205 would play a role, given that those were to occur in ultrathin membranes and thus together with 206 intrinsic barriers. 42 To provide at least a rough answer to this question, we perform a rule of thumb assessment in the following. 208

The rating compares the different effects by computing the associated permeabilites and by 209 defining a reference value that corresponds to the limiting case of diffusion-controlled transport 210 $(\alpha \propto D_{\rm S})$. Subsequent introduction of impact factors permits a quantitative assessment of the different effects' relative importance because the strength of a certain effect scales directly with the 212 associated surface permeability (Supporting Information SI4 for more details). It turns out that the impact of intrinsic surface barriers vary between 1.5 (almost pure diffusion control observed for high θ and T) to 70 (low θ and T). An upper bound for the defect-barrier impact was determined to be ≈2000. The simultaneous occurrence of intrinsic barriers and defects leads to a total surface-barrier impact factor of 2000...40000. Clearly, when both effects appear together the 217 defects excert a stronger influence on the surface barriers than the intrinsic barriers because of the exceptionally large number of closed entrances. However, such a high fraction (99.95%) as observed by Hibbe *et al.* for MOF Zn(tbip)⁶ is unlikely to occur for the broad AFI pore entrances too (Supporting Information SI4). Furthermore, efficient and effective applications implementating ultrathin membranes (e.g., gas separation, heterogeneous catalysis) usually require high accessibility of guest molecules to the zeolite pores, pointing at improvements of corresponding post-synthesis treatment of the membranes in question.

25 Conclusions

Besides highlighting the need for new integral diffusion solutions, the present work provides an accurate prediction of the local transport coefficient that prevails at solid-gas interfaces: the surface permeability. In this respect, the realization that latest improvements in synthesis enable the production of ultrathin and highly oriented zeolite films ³⁷ enhances the significance of the here reported slow boundary layer transport. This is, because the importance of surface barriers scales inversely with membrane width. ²⁰ As a final consequence, simple design protocols, such as membrane selectivity formulae on the mere basis of adsorption data and diffusion coefficients, are becoming increasingly inappropriate for the new generation of ultrathin membranes, calling for development of more accurate design models.

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Associated Content

- Supporting Information Available: Detailed description of two-scale simulation methodology,
- ²⁴³ complementary results, crystal structure, list of symbols; movie illustrating tracer release. This
- material is available free of charge via the Internet at http://pubs.acs.org.

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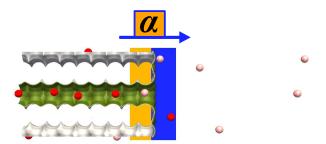
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